MSC IN ANALYSIS AND DESIGN OF EARTHQUAKE RESISTANT STRUCTURES (ADERS)

Course: Geotechnical Engineering in the Design of Structures

PROJECT: SETTLEMENT CALCULATIONS FOR THE LEANING TOWER OF PISA

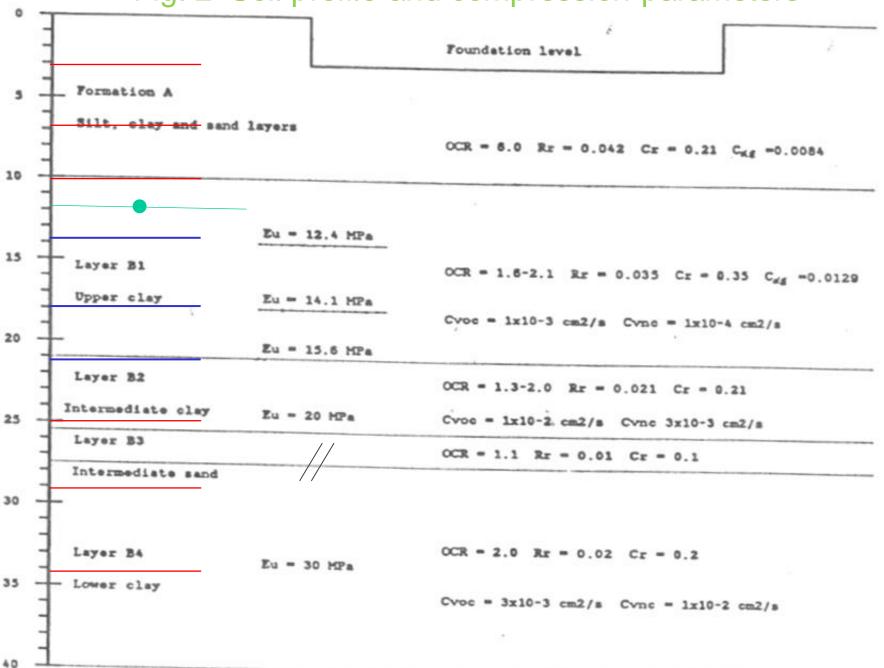
The leaning Tower of Pisa was designed as a circular bell tower of 19.06m in diameter. The tilt of the Tower (before the period of strengthening 1990-2001) is shown in Fig. 1. The first stage of construction took place in the period 1173-1178 and the load applied by three floors to the foundation was 92904kN. Settlement was introduced during this stage.

The second stage of construction took place in the period 1272-1278 and the total load applied to the foundation was 134534kN.

The third stage of construction in the period 1360-1370 resulted in total load of 141640kN.

Calculate the settlement of the Tower until 1990 when a multinational task force of engineers started work on its stabilization. The soil profile and the parameters required for settlement calculations are given in Figs 2,3 and 4.

Fig. 2 Soil profile and compression parameters



$$E_u = \frac{\Delta\sigma}{\varepsilon_z}$$

Immediate settlement, ρ_i

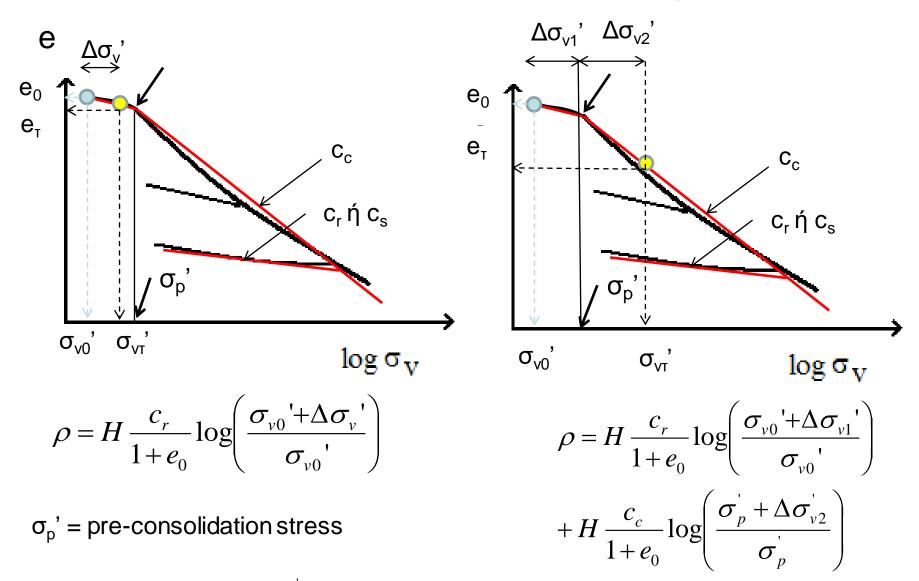
$$\rho = H \frac{c_r}{1 + e_0} \log \left(\frac{\sigma_{v0}' + \Delta \sigma_{v}'}{\sigma_{v0}'} \right)$$

Consolidation settlement, ρ_c

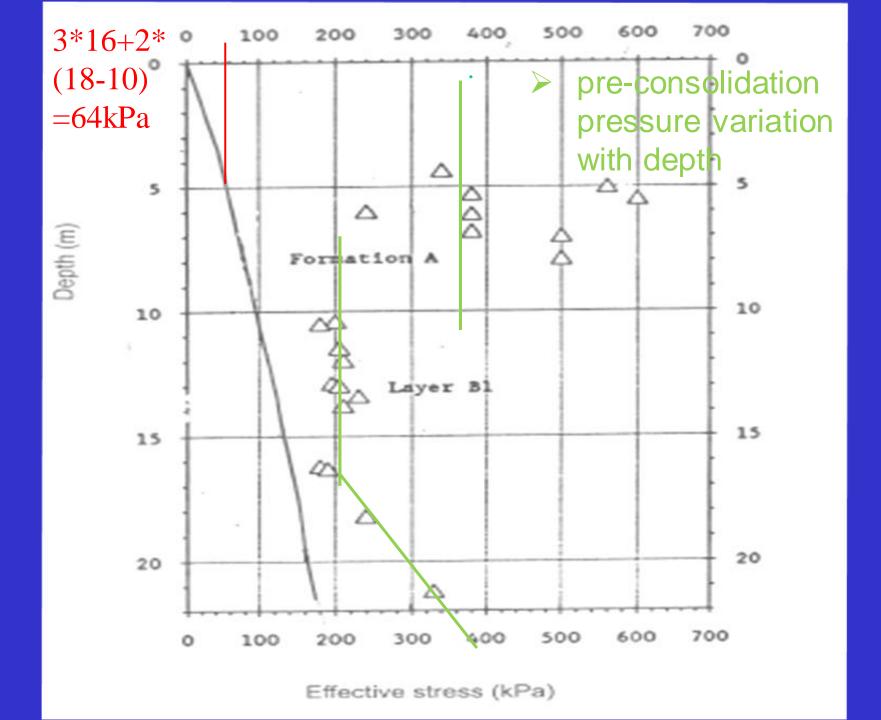
 $\delta_s = h_s C_{\alpha\epsilon} \log_{10}(t/t_s)$ where $t_s = time of$ completion of primary consolidation, h_s =depth of layer at the beginning of secondary consolidation

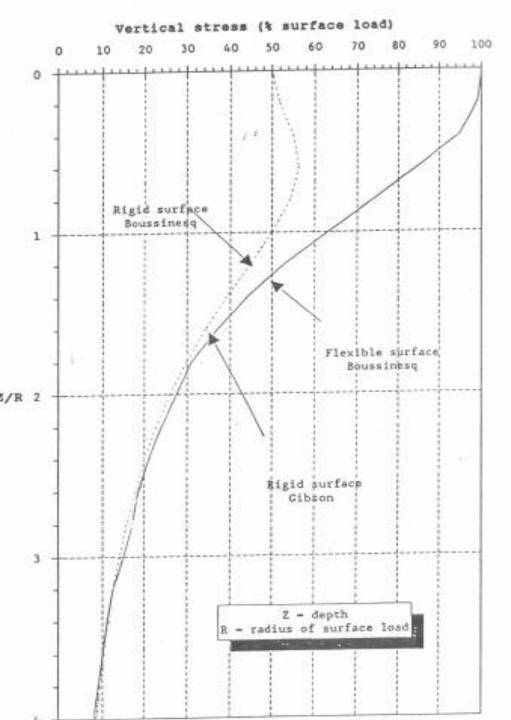
Secondary settlement, ρ_s

Consolidation settlement pc



$$\sigma_{v0} < \sigma_p$$
, $OCR = \frac{\sigma_p}{\sigma_{v0}}$

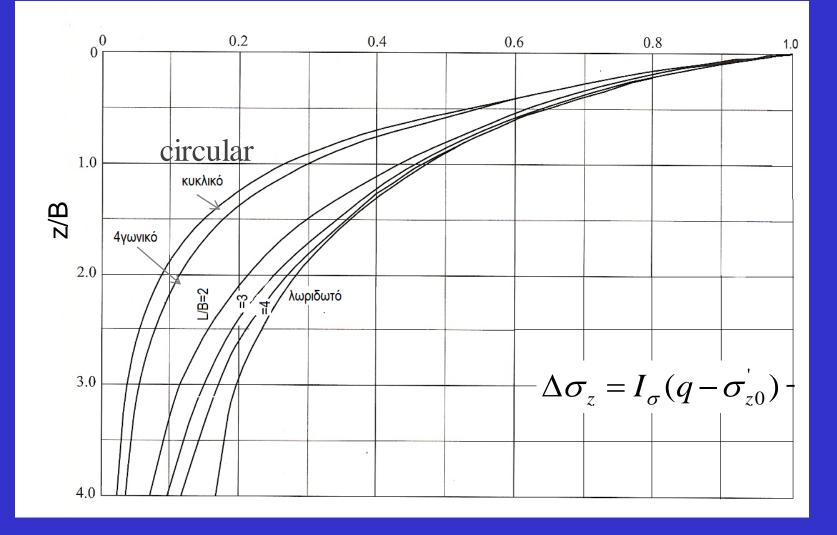




Vertical stress distribution with depth under circular foundation

$$\Delta \sigma_{z} = \left[1 - \left(\frac{1}{1 + \left(\frac{B}{2z} \right)^{2}} \right)^{a} \right] (q - \sigma_{z0})$$

Poulos & Davis 1974 used Boussinesq's equations to calculate stresses on the centre line under a circular footing (α =2.6, B=width of footing)



Stresses under the centre line of rigid footing (Butterfield & Banerjee 1971)



 σ_{z0} '=normal effective stress at depth D